

Design of Cascade-Form IIR Filters with Powers-of-Two Coefficients Using Mixed Integer Linear Programming

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Abstract - We propose an optimal design method for digital IIR filters with powers-of-two coefficients. This method is based upon the formulation of a linear optimization problem that minimizes filter's complexity for given specifications. It is shown that by taking the logarithm to the transfer function of cascade-form IIR filters, the design problem becomes linear and can be solved by mixed integer linear programming (MILP). Design examples are presented to demonstrate the efficiency of the proposed method.

I. INTRODUCTION

One approach to multiplier free digital filter design is to choose filter coefficients from a discrete set consisting of powers-of-two and sums of a few powers-of-two terms. Design methods based on this approach have been developed for FIR filters [1]-[5] and 2-D IIR filters [6],[7].

In this paper, we consider the design of cascade-form 1-D IIR filters with powers-of-two coefficients. Our objective is to develop an optimal procedure for designing such filters with *minimal* complexity, for the specification at hand. By taking the logarithm to the transfer function of a cascade-form IIR filters, we formulate an optimization problem with a linear objective function and linear constraints. Then this problem is solved by MILP. Design examples demonstrate that this method leads to very efficient cascade-form IIR filters with powers-of-two coefficients, which are particularly suitable for VLSI implementation.

II. PROBLEM FORMULATION

Consider the following cascade-form transfer function

$$H(z) = K \frac{\prod_{p=1}^P (1 \pm z^{-1})^{l_p} \prod_{q=1}^Q (1 + a_q z^{-1} + z^{-2})^{m_q}}{\prod_{r=1}^R (1 + c_r z^{-1} + d_r z^{-2})^{n_r}} \quad (1)$$

where a_q, c_r, d_r are sum of powers-of-two coefficients and l_p, m_q and n_r are nonnegative integers. To simplify notation, we define $L_p(z) = (1 \pm z^{-1})^{l_p}$, $N_q(z) = (1 + a_q z^{-1} + z^{-2})^{m_q}$ and $D_r(z) = (1 + c_r z^{-1} + d_r z^{-2})^{n_r}$. Since the word length of a_q, c_r and d_r is finite, the number of all possible $N_q(z)$ and $D_r(z)$ are finite. Given the desired filter specifications, we determine sets of eligible polynomials by examining each possible $L_p(z), N_q(z)$ and $D_r(z)$ based on the following criteria: (i) Roots of $L_p(z)$ and $N_q(z)$ should lie in stopbands. (ii) Roots of $D_r(z)$ should be located within the unit circle, and should not lie in stopbands. In (1), the number of eligible $L_p(z), N_q(z)$ and $D_r(z)$, respectively, are denoted by P, Q and R . Our objective is to find optimal l_p, m_q and n_r values for all eligible $L_p(z), N_q(z)$ and $D_r(z)$. Note that all zeros of $H(z)$ lie on the unit circle. This fact leads to efficient implementation at the expense of some limitation in reducing passband ripple size [8].

Let α_q and β_r be the number of adders required to implement the polynomials $N_q(z)$ and $D_r(z)$, respectively. For example, when the coefficients a_1, c_1 and d_1 are sum of two powers-of-two terms, we get $\alpha_1 = 3, \beta_1 = 4$. Note that the number of adders for realizing $L_p(z)$ is always one. Now an IIR filter, represented by (1), with minimal complexity may be designed by solving the following

the following optimization problem. For a given passband ripple δ_p and stopband ripple δ_s :

$$\begin{aligned}
\text{Minimize } & v = A_{num} + A_{den} && \text{(measure of complexity)} \\
\text{Subject to } & \left| |H(\omega)| - H_d(\omega) \right| < \delta_p && \text{(in passbands)} \\
& |H(\omega)| < \delta_s && \text{(in stopbands)} \\
& \sum_{p=1}^P l_p + \sum_{q=1}^Q \alpha_q \bullet m_q = A_{num} && \text{(No. of adders in numerator)} \\
& \sum_{r=1}^R \beta_r \bullet n_r = A_{den} && \text{(No. of adders in denominator)}
\end{aligned} \tag{2}$$

where A_{num} and A_{den} denote the total number of adders in the numerator and the denominator, respectively, and $H_d(\omega)$ is the desired magnitude response. This design problem requires some nonlinear optimization technique due to the nonlinearity of $H(\omega)$. However, by taking the logarithm on $H(\omega)$, this can be converted into a linear problem. We define

$$\begin{aligned}
H_{dB}(\omega) &= 20 \log |H(\omega)| \\
&= K_{dB} + \sum_{p=1}^P l_p L_{p dB}(\omega) \\
&\quad + \sum_{q=1}^Q m_q N_{q dB}(\omega) - \sum_{r=1}^R n_r D_{r dB}(\omega)
\end{aligned} \tag{3}$$

where $K_{dB} = 20 \log |K|$, $L_{p dB}(\omega) = 20 \log |L_p(\omega)|$, $N_{q dB}(\omega) = 20 \log |N_q(\omega)|$ and $D_{r dB}(\omega) = 20 \log |D_r(\omega)|$. Now the optimization in (2) can be rewritten as

$$\begin{aligned}
\text{Minimize } & v = A_{num} + A_{den} && \text{(measure of complexity)} \\
\text{Subject to } & 20 \log \left(1 - \frac{\delta_p}{H_d(\omega)} \right) && \text{(in passbands)} \\
& < H_{dB}(\omega) - 20 \log H_d(\omega) \\
& H_{dB}(\omega) - 20 \log H_d(\omega) && \text{(in passbands)} \\
& < 20 \log \left(1 + \frac{\delta_p}{H_d(\omega)} \right) \\
& H_{dB}(\omega) < 20 \log \delta_s && \text{(in stopbands)} \\
& \sum_{p=1}^P l_p + \sum_{q=1}^Q \alpha_q \bullet m_q = A_{num} && \text{(No. of adders in numerator)} \\
& \sum_{r=1}^R \beta_r \bullet n_r = A_{den} && \text{(No. of adders in denominator)}
\end{aligned} \tag{4}$$

This problem can be solved by MILP, treating K_{dB} , l_p , m_q , and n_r as variables. The proposed design algorithm is summarized as follows:

Step 1. Determine the sets of eligible

polynomials following the procedure stated below (1).

Step 2. Determine K_{dB} , l_p , m_q , n_r by solving the optimization problem in (4).

III. DESIGN EXAMPLES

To compare the proposed design methods with the previous ones, our method is applied to the filter design problems considered in [9] and [10]. The design problems were solved in a Sparc 20 workstation using the commercial general purpose MILP package in [11].

Example 1 (Lowpass filter): The specifications in normalized frequency are:

passband: $F \in [0, 0.2]$, stopband: $F \in [0.3, 0.5]$

ripple: $\delta_p \leq 0.1 \text{ dB}$ in passband,

$\delta_s \geq 33 \text{ dB}$ in stopband.

In [9] an IIR filter with 6 bits coefficients, requiring multipliers for its implementation, was designed under these specifications. In our design, we assume that filter coefficients are sum of two powers-of-two terms and that each powers-of-two term consists of 6 bits including sign bit. The number of eligible polynomials are: $P=1$, $Q=10$, $R=280$. The design time was approximately 10 minutes. Fig. 1 shows the magnitude response of the resulting filter, and Table I compares the results of the proposed method with those of [9]. It is seen that our design reduced 15 multipliers and 2 adders, while resulting in smaller passband ripple and greater stopband attenuation. The proposed technique, which leads to multiplier-free implementation, can yield better and simpler IIR filters than can the method in [9] which requires multipliers.

Example 2 (Bandpass filter): The specifications in normalized frequency are:

passband: $F \in [0.125, 0.175]$,

stopband: $F \in [0, 0.105] \cup [0.195, 0.5]$

ripple: $\delta_p \leq 0.2 \text{ dB}$ in passband,

$\delta_s \geq 40 \text{ dB}$ in stopband.

In [10] an IIR filter employing cyclotomic numerator polynomials, which leads to multiplierless numerator implementation, and denominator polynomials with infinite precision coefficients, was designed under these specifications. In this case, we assume that filter coefficients are sum of *three* powers-of-two terms. Again, each powers-of-two term consists of 6

bits. The number of eligible polynomials are: $P=2$, $Q=31$, $R=142$. The design time was approximately 15 minutes. Fig. 2 shows the magnitude response of the resulting filter, and the last two columns of Table I compares the results of the proposed method with those in [10]. Our design eliminated the need of 9 infinite precision multipliers at the expense of 17 additional adders. The proposed technique leads to simpler IIR filters requiring only shifters and 6 bits adder than can the method in [10] which requires infinite precision multipliers and adders.

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Table I. Comparison and Summary of the Examples

Examples	Lowpass filter		Bandpass filter	
	[9]	Proposed	[10]	Proposed
No. of adder	12	10	16	33
No. of multiplier	15	-	9	-
Passband ripple(dB)	0.09	0.082	0.2	0.18
Stopband attenuation(dB)	33.58	38.7	42.1	40.5

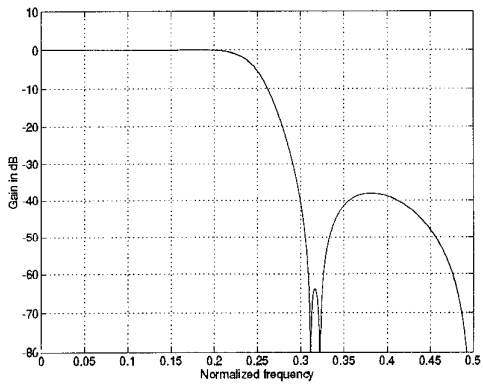


Figure 1. Magnitude response of the designed filter of example 1.

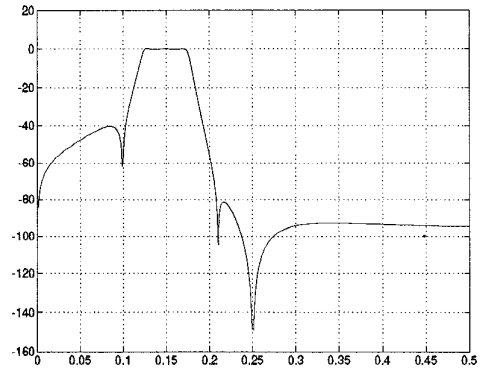


Figure 2. Magnitude response of the designed filter of example 2.